

OPTIMAL DISTRIBUTION OF ACTIVE LOAD IN POWER SYSTEM CONSIDERING THE SERIES OF HYDROPOWER PLANTS

G.MAKHARADZE, T.JIKIA

Optimal distribution of the active load in the power system considering the series of hydropower plants is reviewed.

Efficiency function, system of the constraint equations and inequalities were drafted based on mathematic expressions of the plant metering characteristics. Lagrange indefinite multiplier method was applied in the problem solution.

An equation system for the problem of the active load distribution optimization between the power plants in the power system taking into the account the seasonal hydropower plants operating in series with the hydropower plants with reservoirs the operation of which is somehow associated with the operating condition of regulating hydropower plants is obtained.

Key words: constraint equations, minimization of fuel consumption, function extremum, active load, balancing thermal plant.

The equation system of the optimization problem connects the engineering-and-economical performance of the production and technological process to the main operation parameters of the unit to be researched. These parameters are the sought parameters of the problem.

Mathematic model for the optimization of any technological process generally contains five equation groups: effectiveness i.e. aim equation, coupling equation, constraint equations and inequalities, optimal management equation, adaptation equation.

Optimal distribution of the active load between hydropower plants is one of the main activities in the power system helping to achieve as small consumption of the primary energy resource as possible. In the power system the problem of minimizing the consumption of the primary energy resource under the conditions of limited (preliminarily determined) water resource arrives to the problem of minimizing the fuel consumption at the thermal plants. In such case, the efficiency function has the following form [1-3]:

$$T = \sum_{k=1}^k \sum_{i=0}^n T_{i,t} \tau_t \Rightarrow \min, \quad (1)$$

Where τ_t is the time interval within which the total power system load can be considered as a constant value (for simplicity $\tau_t = 1\text{hr}$ is usually taken); $k - \tau_t$ is the total amount of the intervals within the involved period; $T_{i,t} - i$ is an hourly fuel consumption in τ_t interval at the thermal plants; $0 -$ index is granted to balancing thermal plant; $n -$ total number of the remainder thermal plants.

Coupling equations are presented by metering characteristics of the power plants in form of second row polynomial [2]:

$$T_{i,t} = T_{0,t} + a_i P_{i,t} + b_i P_{i,t}^2 \quad (\text{kg/h}); \quad i = 0, 1, 2, \dots, n \quad (2)$$

and

$$Q_{j,t} = Q_{0,j} + a_j P_{j,t} + b_j P_{j,t}^2 \quad (\text{m}^3/\text{sec}); \quad j = \alpha, \beta, \mu. \quad (3)$$

Here, $T_{i,t} - i$ is an hourly fuel consumption at the thermal plant; $Q_{j,t} - i$ is the total water consumption at the hydropower plant; $P_{i,t} -$ load of the thermal plants at τ_t interval; $P_{j,t} -$ load of the hydropower plants at τ_t interval; $T_{0,t}, Q_{0,j}, a_i, b_i, a_j, b_j -$ polynomial coefficients; $\mu -$ total number of the hydropower plants.

The following is considered in form of the constraint equations:

- active capacity balance equation for each τ_t interval

$$W_{p,t} = \sum_{i=0}^n P_{i,t} + \sum_{j=\alpha}^m P_{j,t} + \sum_{Q_{0,t} \leq Q_{0,t} - P_{Q_{0,t}}} - P_{Q_{0,t}} = 0, \quad (4)$$

Where $P_{\text{remainder plants } t}$ – total load of the remainder power plants operating in the system including the seasonal hydropower plants operating in series with regulating hydropower plants the operating condition of which is somehow associated with the operating condition of the regulating hydropower plants; m – total number $m < \mu$ of regulating (having reservoirs) hydropower plants;

- daily water limit for particular regulating hydropower plants

$$W_{Q,j} = 3600 \cdot \sum_{t=1}^{24} Q_{j,t} \tau_t - Q_{j,\text{lim}} = 0 \quad j = \alpha, \beta \dots m \quad (5)$$

Where, $Q_{j,\text{lim},j}$ is daily water limit (m^3/d) for the hydropower plant.

As a coupling inequality we have:

$$P_{i,\text{dan}} \leq P_i \leq P_{i,\text{sadg}} \quad \text{and} \quad P_{j,\text{dan}} \leq P_j \leq P_{j,\text{sadg}}. \quad (6)$$

Optimal management, i.e. optimization equation allows to conduct the optimal process management. It is obtained by joint consideration of the aim, coupling and constraint equations and is the link between the sought variables and the aim of the optimization problem.

In the solution of the optimization problems Lagrange indefinite multiplier method is used. Here, instead of the efficiency function extremum written in (1) form the Lagrange function extremum is considered and written in a following form:

$$L = T + \lambda_{\tau} W_{p,t} + \sum_{j=\alpha}^m \lambda_j W_{Q,j} \Rightarrow \min,$$

i.e.

$$\begin{aligned} L = & \sum_{t=1}^{24} \sum_{i=0}^n (T_{0,i,t} + a_i P_{i,t} + b_i P_{i,t}^2 + \\ & + \sum_{i=1}^{24} \lambda_{\tau} (\sum_{i=0}^n P_{i,t} + \sum P_{\text{dan.sadg},t} - \\ & - P_t - \Delta P) + \sum_{j=\alpha}^m \lambda_j [3600 \sum_{t=1}^{24} (Q_{0,j,t} + a_j P_{j,t} + b_j P_{j,t}^2) - Q_{j,\text{lim}}] \Rightarrow \min. \end{aligned} \quad (7)$$

In this expression $\tau_t=1$, and $\lambda_{\tau}, \lambda_j$ are the multiplication of the Lagrange indefinite multipliers.

By differentiating the Lagrange function (7) with P_i and P_j will get:

$$\left. \begin{aligned} \frac{\partial L}{\partial P_{0,t}} &= s_{0,t} + \lambda_{\tau} \left(1 - \frac{\partial \Delta P}{\partial P_{0,t}} \right) = 0 \\ \frac{\partial L}{\partial P_{1,t}} &= s_{1,t} + \lambda_{\tau} \left(1 - \frac{\partial \Delta P}{\partial P_{1,t}} \right) = 0 \\ \frac{\partial L}{\partial P_{i,t}} &= s_{i,t} + \lambda_{\tau} \left(1 - \frac{\partial \Delta P}{\partial P_{i,t}} \right) = 0 \\ \frac{\partial L}{\partial P_{n,t}} &= s_{n,t} + \lambda_{\tau} \left(1 - \frac{\partial \Delta P}{\partial P_{n,t}} \right) = 0 \end{aligned} \right\} \quad (8)$$

and

$$\left. \begin{aligned} \frac{\partial L}{\partial P_{\alpha,t}} &= \lambda_t \left(1 - \frac{\partial \Delta P}{\partial P_{\alpha,t}} \right) + 3600 \lambda_{\alpha,t} \varepsilon_{\alpha,t} = 0 \\ \frac{\partial L}{\partial P_{\beta,t}} &= \lambda_t \left(1 - \frac{\partial \Delta P}{\partial P_{\beta,t}} \right) + 3600 \lambda_{\beta,t} \varepsilon_{\beta,t} = 0 \\ &\vdots \\ \frac{\partial L}{\partial P_{j,t}} &= \lambda_t \left(1 - \frac{\partial \Delta P}{\partial P_{j,t}} \right) + 3600 \lambda_{j,t} \varepsilon_{j,t} = 0 \\ &\vdots \\ \frac{\partial L}{\partial P_{m,t}} &= \lambda_t \left(1 - \frac{\partial \Delta P}{\partial P_{m,t}} \right) + 3600 \lambda_{m,t} \varepsilon_{m,t} = 0 \end{aligned} \right\} \quad (9)$$

According to the sought variables $P_{\alpha,t}$ and $P_{j,t}$ the function minimization requirement provides the following equation system:

$$\begin{aligned} \varepsilon_{i,t} + \lambda_t &= 0 & i &= 1, 2, \dots, n \\ \lambda_t + 3600 \lambda_{j,t} \varepsilon_{j,t} &= 0 & j &= \alpha, \dots, m. \end{aligned}$$

After excluding λ_t indefinite multiplier in the derived equation system, will get that the necessary condition for the optimal distribution of the active load between the plants is the equality of relative increments of their primary energy resource.

$$\varepsilon_{1,t} = \varepsilon_{2,t} = \dots \varepsilon_{n,t} = 3600 \lambda_{\alpha} \varepsilon_{\alpha,t} = 3600 \lambda_{\beta} \varepsilon_{\beta,t} = \dots = 3600 \lambda_m \varepsilon_{m,t} = \varepsilon_0 \quad (10)$$

$$\text{i.e.} \quad \left. \begin{aligned} \varepsilon_1 &= \varepsilon_0 \\ \varepsilon_2 &= \varepsilon_0 \\ &\vdots \\ \varepsilon_n &= \varepsilon_0 \\ 3600 \lambda_{\alpha} \varepsilon_{\alpha} &= \varepsilon_0 \\ &\vdots \\ 3600 \lambda_m \varepsilon_m &= \varepsilon_0 \end{aligned} \right\}.$$

(4), (5) and (10) equations jointly represent the equation system, which in form of (6) considering the inequality allows to resolve the set problem.

λ_j multiplier included in this equation system represents the relation between the fuel consumption at balancing thermal plant and water consumption at j regulating hydropower plant. In particular, λ_j shows how (in what quantity) the fuel consumption (kg) at balancing thermal plant changes in case of changing the water consumption at j regulating hydropower plant by one unit (m^3). For given hydropower plant it is called the efficiency coefficient of water resource.

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